## 2 System Modeling Diagrams

- Graphical simplification using the TF is easier and more informative than algebraic manipulation
- See the figure 3.9 for series, parallel, and feedback manipulations



• The gain of a single-loop negative feedback system is given by the forward gain divided by the sum of 1 plus the loop gain

$$Y(s) = \frac{G_1(s)}{1 + G_2(s)G_1(s)}R(s)$$

• See the figure 3.10 for conversions







• A system without a component in the feedback path is referred to as a unity feedback system

• (Example 3.22, TF from a Simple Block Diagram) Find the TF of the system shown in Fig. 3.11



$$T(s) = \frac{Y(s)}{R(s)} = \frac{\frac{1}{s}(2+\frac{4}{s})}{1+\frac{1}{s}(2+\frac{4}{s})} = \frac{2s+4}{s^2+2s+4}$$

• (Example 3.23, TF from the Block Diagram) Find the TF of the system shown in Fig. 3.12











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• (Example 3.24, TF of a Simple System using Matlab Simulink) Find the TF of the system shown in Fig. 3.13 with  $G_1(s) = 2$ ,  $G_2(s) = \frac{4}{s}$ ,  $G_4(s) = \frac{1}{s}$  and  $G_6(s) = 1$ 



• Mason's rule is useful technique for determining TFs of complicated interconnected systems. (out of the scope of the textbook, but you can get materials in Appendix W3.2.3 online at www.pearsonglobaleditions.com)

## **3** Effect of Pole Locations

- 1. Real Poles
  - Consider the following simple TF

$$H(s) = \frac{1}{s+\sigma}$$

where the pole is located at  $s = -\sigma$  since it is the point where H(s) is infinity.

• The impulse response of the TF is

$$h(t) = e^{-\sigma t}$$
 for  $t \ge 0$ 

- When  $\sigma > 0$ , the pole is located at s < 0, the exponential expression decays and we say the impulse response is "stable"
- If  $\sigma < 0$ , the pole is to the right of the origin. Because the exponential expression here grows with time, the impulse response is referred to as "unstable".



• Let us introduce the time constant

$$au = \frac{1}{\sigma} \qquad \leftarrow \qquad h(t) = e^{-\sigma t} = e^{-\frac{t}{\tau}} \quad \text{for} \quad t \ge 0$$

• The time constant is a measure of the rate of decay (or a measure for the speed of response of the system). The straight line is tangent to the exponential curve at t = 0 and terminates  $t = \tau$ . For example, 63% at  $t = \tau$ , 86% at  $t = 2\tau$ , 95% at  $t = 3\tau$ , 98% at  $t = 4\tau$ , and 99% at  $t = 5\tau$ .

• (Example 3.25, Real Roots) Discuss about the impulse response of the following system:

$$H(s) = \frac{2s+1}{s^2+3s+2}$$

- a) poles: s = -1 and s = -2 since they are points that  $H(s) = \infty$
- b) zeros: s = -0.5 and  $s = \infty$  since they are points that H(s) = 0
- c) partial fraction expression:

$$H(s) = \frac{2s+1}{(s+1)(s+2)} = \frac{-1}{s+1} + \frac{3}{s+2}$$

d) impulse response:

$$h(t) = 3e^{-2t} - e^{-t}$$
 for  $t \ge 0$ 



A sketch of these pole locations and corresponding natural responses is given in Fig. 3.16, along with other pole locations including complex ones.



- a) Poles farther to the left in the s-plane are associated with natural signals that decay faster than those associated with poles closer to the imaginary axis.
- b) In the response of  $h(t) = 3e^{-2t} e^{-t}$ , the fast  $3e^{-2t}$  term dominates the early part of the time history and the  $-e^{-t}$  term is the primary contributor later on.

- 2. Complex Poles
  - Consider the typical second-order system with  $0 < \zeta < 1$  :

$$H(s) = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$
$$= \frac{\omega_n^2}{(s + \zeta\omega_n)^2 + \omega_n^2(1 - \zeta^2)}$$

- a) complex poles :  $s = -\zeta \omega_n \pm j \omega_n \sqrt{1-\zeta^2}$
- b) damping ratio :  $\zeta$
- c) Neper frequency :  $\sigma = \zeta \omega_n$
- d) undamped natural frequency :  $\omega_n$
- e) damped natural frequency :  $\omega_d = \omega_n \sqrt{1-\zeta^2}$
- f) The poles of this TF are located at a radius  $\omega_n$  in the s-plane and at an angle  $\theta = \sin^{-1} \zeta$ , as shown in Figs. 3.18 and 3.20



• Impulse response becomes

$$H(s) = \frac{\omega_n^2}{(s+\zeta\omega_n)^2 + \omega_n^2(1-\zeta^2)}$$
  
=  $\frac{\omega_n^2}{\omega_d} \frac{\omega_d}{(s+\zeta\omega_n)^2 + \omega_d^2}$   
=  $\frac{\omega_n}{\sqrt{1-\zeta^2}} \frac{\omega_d}{(s+\zeta\omega_n)^2 + \omega_d^2} \rightarrow \mathcal{L}[e^{-\sigma t}f(t)] = F(s+\sigma)$   
 $h(t) = \frac{\omega_n}{\sqrt{1-\zeta^2}} e^{-\zeta\omega_n t} \sin \omega_d t \quad \text{for} \quad t \ge 0$ 

a) Actual frequency  $\omega_d$  decreases slightly as the damping ratio increases

b) Negative real part of the pole  $\sigma = \zeta \omega_n$  determines the decay rate of an exponential envelope  $(\frac{\omega_n}{\sqrt{1-\zeta^2}}e^{-\zeta\omega_n t})$  and  $-\frac{\omega_n}{\sqrt{1-\zeta^2}}e^{-\zeta\omega_n t}$  that multiplies the sinusoid as shown in Fig. 3.21



## • Stability

- a) If  $\sigma < 0$  (and the pole is in the RHP), then the natural response will grow with time, so, as defined earlier, the system is said to be unstable.
- b) If  $\sigma = 0$ , the natural response neither grows nor decays, so stability is open to debate.
- c) If  $\sigma > 0$ , the natural response decays, so the system is stable.

• (Example 3.26, Oscillatory Time Response) Discuss the correlation b/w the poles and impulse response of the system:

$$H(s) = \frac{2s+1}{s^2+2s+5} = \frac{2s+1}{(s+1)^2+2^2}$$
$$= 2\frac{s+1}{(s+1)^2+2^2} - \frac{1}{2}\frac{2}{(s+1)^2+2^2}$$
$$h(t) = 2e^{-t}\cos 2t - \frac{1}{2}e^{-t}\sin 2t \quad \text{for } t \ge 0$$
$$= \frac{\sqrt{17}}{2}e^{-t}\cos\left(2t + \tan^{-1}\frac{1}{4}\right)$$

a) 
$$\omega_n = \sqrt{5} = 2.24$$
 from  $\omega_n^2 = 5$   
b)  $\zeta = \frac{1}{\sqrt{5}} = 0.447$  from  $2\zeta\omega_n = 2$   
c)  $\omega_d = 2$  from  $\omega_d = \omega_n \sqrt{1 - \zeta^2}$   
d) both envelopes are  $\frac{\sqrt{17}}{2}e^{-t}$  and  $-\frac{\sqrt{17}}{2}e^{-t}$   
e) impulse response is plotted in Fig. 3.22

