

# Solutions of Final Exam

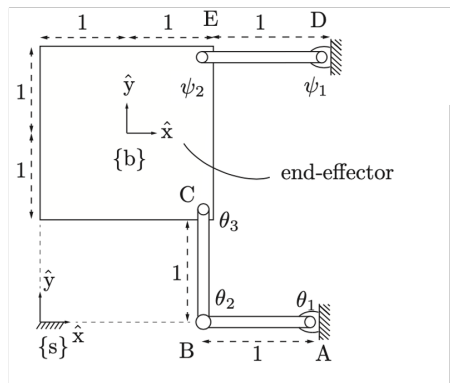
Subject : Modern Robotics, Lecturer : Prof. Youngjin Choi,

Date : June 18, 2020 (Contact e-mail : cyj@hanyang.ac.kr)

Notice that the answers should be written only in English, otherwise you will get a zero point.

**Problem 1 (30pt)** Assume a five-bar linkage is in its zero position. Let  $(p_x, p_y)$  be the position of the {b}-frame origin expressed in {s}-frame coordinates, and let  $\phi$  be the orientation of the {b} frame. Find the forward kinematics Jacobian  $J_a$  from  $\mathcal{V}_s = J_a \dot{q}_a$  when  $B, D$  are actuated, i.e.  $\dot{q}_a = (\dot{\theta}_2, \dot{\psi}_1)$  and  $\dot{q}_p = (\dot{\theta}_1, \dot{\theta}_3, \dot{\psi}_2)$ . You may make

use of the matrix inversion of 
$$\begin{bmatrix} 1 & 1 & -1 \\ 0 & 1 & -3 \\ -3 & -2 & 2 \end{bmatrix}^{-1} = \begin{bmatrix} -2 & 0 & -1 \\ 4.5 & -0.5 & 1.5 \\ 1.5 & -0.5 & 0.5 \end{bmatrix}.$$



**Solution of Problem 1 (30pt)** Since

$$\begin{aligned} \mathcal{V}_s &= J_1 \dot{\theta} = J_2 \dot{\psi} \\ &= \begin{bmatrix} 1 & 1 & 1 \\ 0 & 0 & 1 \\ -3 & -2 & -2 \end{bmatrix} \begin{bmatrix} \dot{\theta}_1 \\ \dot{\theta}_2 \\ \dot{\theta}_3 \end{bmatrix} = \begin{bmatrix} 1 & 1 \\ 3 & 3 \\ -3 & -2 \end{bmatrix} \begin{bmatrix} \dot{\psi}_1 \\ \dot{\psi}_2 \end{bmatrix} \end{aligned}$$

we can obtain the following relations

$$\begin{aligned} J_1 \dot{\theta} - J_2 \dot{\psi} &= 0 & H_a \dot{q}_a + H_p \dot{q}_p &= 0 \\ \begin{bmatrix} 1 & 1 & 1 & -1 & -1 \\ 0 & 0 & 1 & -3 & -3 \\ -3 & -2 & -2 & 3 & 2 \end{bmatrix} \begin{bmatrix} \dot{\theta}_1 \\ \dot{\theta}_2 \\ \dot{\theta}_3 \\ \dot{\psi}_1 \\ \dot{\psi}_2 \end{bmatrix} &= \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} & \begin{bmatrix} 1 & -1 \\ 0 & -3 \\ -2 & 3 \end{bmatrix} \begin{bmatrix} \dot{\theta}_2 \\ \dot{\psi}_1 \end{bmatrix} + \begin{bmatrix} 1 & 1 & -1 \\ 0 & 1 & -3 \\ -3 & -2 & 2 \end{bmatrix} \begin{bmatrix} \dot{\theta}_1 \\ \dot{\theta}_3 \\ \dot{\psi}_2 \end{bmatrix} &= \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \end{aligned}$$

Now, we have

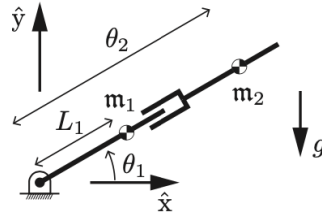
$$\dot{q}_p = -H_p^{-1} H_a \dot{q}_a$$
$$\begin{bmatrix} \dot{\theta}_1 \\ \dot{\theta}_3 \\ \dot{\psi}_2 \end{bmatrix} = - \begin{bmatrix} -2 & 0 & -1 \\ 4.5 & -0.5 & 1.5 \\ 1.5 & -0.5 & 0.5 \end{bmatrix} \begin{bmatrix} 1 & -1 \\ 0 & -3 \\ -2 & 3 \end{bmatrix} \begin{bmatrix} \dot{\theta}_2 \\ \dot{\psi}_1 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -1.5 & -1.5 \\ -0.5 & -1.5 \end{bmatrix} \begin{bmatrix} \dot{\theta}_2 \\ \dot{\psi}_1 \end{bmatrix}$$

Thus

$$\begin{aligned} \mathcal{V}_s &= J_1 \dot{\theta} \\ &= \begin{bmatrix} 1 & 1 & 1 \\ 0 & 0 & 1 \\ -3 & -2 & -2 \end{bmatrix} \begin{bmatrix} \dot{\theta}_1 \\ \dot{\theta}_2 \\ \dot{\theta}_3 \end{bmatrix} \\ &= \begin{bmatrix} 1 & 1 & 1 \\ 0 & 0 & 1 \\ -3 & -2 & -2 \end{bmatrix} \begin{bmatrix} 0 & 1 \\ 1 & 0 \\ -1.5 & -1.5 \end{bmatrix} \begin{bmatrix} \dot{\theta}_2 \\ \dot{\psi}_1 \end{bmatrix} \\ &= \begin{bmatrix} -0.5 & -0.5 \\ -1.5 & -1.5 \\ 1 & 0 \end{bmatrix} \begin{bmatrix} \dot{\theta}_2 \\ \dot{\psi}_1 \end{bmatrix} \\ &= J_a \dot{q}_a \end{aligned}$$

**Problem 2 (40pt)** The figure illustrates an RP robot moving in a vertical plane. The mass of link 1 is  $m_1 = 1[kg]$  and the center of mass is a distance  $L_1 = 1[m]$  from joint 1. The scalar inertia of link 1 about an axis through the center of mass and out of the plane is  $\mathcal{I}_1 = 1[kg \cdot m^2]$ . The mass of link 2 is  $m_2 = 1[kg]$ , the center of mass is a distance  $\theta_2$  from joint 1, and the scalar inertia of link 2 about its center of mass is  $\mathcal{I}_2 = 1[kg \cdot m^2]$ . Gravity  $g$  acts downward on the page. Derive the equation of motion ?

$$M(\theta)\ddot{\theta} + c(\theta, \dot{\theta}) + g(\theta) = \tau$$



**Solution of Problem 2 (40pt)** Positions of the center of mass of link  $i$

$$x_1 = L_1 \cos \theta_1 = \cos \theta_1 \quad y_1 = L_1 \sin \theta_1 = \sin \theta_1 \quad x_2 = \theta_2 \cos \theta_1 \quad y_2 = \theta_2 \sin \theta_1$$

Velocities of the center of mass of link  $i$

$$\dot{x}_1 = -\dot{\theta}_1 \sin \theta_1 \quad \dot{y}_1 = \dot{\theta}_1 \cos \theta_1 \quad \dot{x}_2 = \dot{\theta}_2 \cos \theta_1 - \theta_2 \dot{\theta}_1 \sin \theta_1 \quad \dot{y}_2 = \dot{\theta}_2 \sin \theta_1 + \theta_2 \dot{\theta}_1 \cos \theta_1$$

Kinetic energies of link  $i$

$$\mathcal{K}_1 = \frac{1}{2} m_1 (\dot{x}_1^2 + \dot{y}_1^2) + \frac{1}{2} \mathcal{I}_1 \dot{\theta}_1^2 = \dot{\theta}_1^2$$

$$\mathcal{K}_2 = \frac{1}{2} m_2 (\dot{x}_2^2 + \dot{y}_2^2) + \frac{1}{2} \mathcal{I}_2 \dot{\theta}_2^2 = \frac{1}{2} \left( (1 + \theta_2^2) \dot{\theta}_1^2 + \dot{\theta}_2^2 \right)$$

Potential energies of link  $i$

$$\mathcal{P}_1 = m_1 g y_1 = g \sin \theta_1$$

$$\mathcal{P}_2 = m_2 g y_2 = g \theta_2 \sin \theta_1$$

Lagrangian becomes

$$\mathcal{L} = \mathcal{K}_1 + \mathcal{K}_2 - \mathcal{P}_1 - \mathcal{P}_2$$

$$= \frac{3}{2} \dot{\theta}_1^2 + \frac{1}{2} \theta_2^2 \dot{\theta}_1^2 + \frac{1}{2} \dot{\theta}_2^2 - g \sin \theta_1 - g \theta_2 \sin \theta_1$$

The Euler-Lagrange equations for this example are of the form

$$\begin{aligned}
 \tau_1 &= \frac{d}{dt} \frac{\partial \mathcal{L}}{\partial \dot{\theta}_1} - \frac{\partial \mathcal{L}}{\partial \theta_1} \\
 &= \frac{d}{dt} (3\dot{\theta}_1 + \theta_2^2 \dot{\theta}_1) + g \cos \theta_1 + g\theta_2 \cos \theta_1 \\
 &= 3\ddot{\theta}_1 + 2\theta_2 \dot{\theta}_2 \dot{\theta}_1 + \theta_2^2 \ddot{\theta}_1 + g \cos \theta_1 + g\theta_2 \cos \theta_1 \\
 \tau_2 &= \frac{d}{dt} \frac{\partial \mathcal{L}}{\partial \dot{\theta}_2} - \frac{\partial \mathcal{L}}{\partial \theta_2} \\
 &= \frac{d}{dt} (\dot{\theta}_2) - \theta_2 \dot{\theta}_1^2 + g \sin \theta_1 \\
 &= \ddot{\theta}_2 - \theta_2 \dot{\theta}_1^2 + g \sin \theta_1
 \end{aligned}$$

Now we can complete the dynamics as follows:

$$M(\theta) \ddot{\theta} + c(\theta, \dot{\theta}) + g(\theta) = \tau$$

$$\begin{bmatrix} 3 + \theta_2^2 & 0 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} \ddot{\theta}_1 \\ \ddot{\theta}_2 \end{bmatrix} + \begin{bmatrix} 2\theta_2 \dot{\theta}_1 \dot{\theta}_2 \\ -\theta_2 \dot{\theta}_1^2 \end{bmatrix} + \begin{bmatrix} (1 + \theta_2)g \cos \theta_1 \\ g \sin \theta_1 \end{bmatrix} = \begin{bmatrix} \tau_1 \\ \tau_2 \end{bmatrix}$$

**Problem 3 (30pt)** For given a one-dof mass-spring-damper system of the form  $m\ddot{x} + b\dot{x} + kx = f$ , where  $f$  is the control force and  $m = 4[\text{kg}]$  and  $b = 2[\text{Ns/m}]$  and  $k = 0.1[\text{N/m}]$ , determine the gains  $k_p$  and  $k_d$  so that the following PD controller

$$f = k_d(\dot{x}_d - \dot{x}) + k_p(x_d - x)$$

can yield the critical damping and the 2% settling time of  $0.01[\text{s}]$ , where  $x_d = 1$  and  $\dot{x}_d = 0$ .

**Solution of Problem 3 (30pt)** Let us obtain the error dynamics using  $x_e = x_d - x$ ,  $\dot{x}_e = -\dot{x}$ , and  $\ddot{x}_e = -\ddot{x}$

$$\begin{aligned} m\ddot{x} + b\dot{x} + kx &= k_d(\dot{x}_d - \dot{x}) + k_p(x_d - x) \\ -m\ddot{x}_e - b\dot{x}_e + k(x_d - x_e) &= k_d\dot{x}_e + k_px_e \\ 4\ddot{x}_e + (k_d + 2)\dot{x}_e + (k_p + 0.1)x_e &= 0.1 \\ \ddot{x}_e + \frac{k_d + 2}{4}\dot{x}_e + \frac{k_p + 0.1}{4}x_e &= 0.025 \end{aligned}$$

From the following relations, we have

$$\omega_n^2 = \frac{k_p + 0.1}{4} \qquad 2\zeta\omega_n = \frac{k_d + 2}{4}$$

Since  $\zeta = 1$  and  $\frac{4}{\zeta\omega_n} = 0.01$ , we have

$$k_p = 639,999.9 \approx 6.4 \times 10^5 \qquad k_d = 3,198$$